

# Static Crossover of Critical Behavior in Polymer Blend Solutions: Scaling Analysis of the Ginzburg Number

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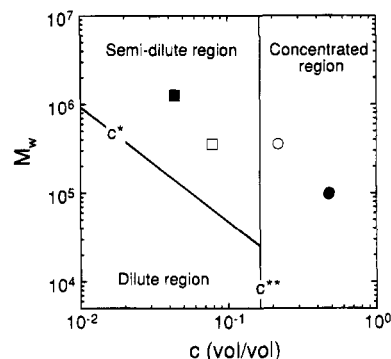
**ABSTRACT:** By means of light scattering, the static critical behavior was investigated for symmetrical polymer blend solutions of polystyrene/poly(methyl methacrylate)/deuterated benzene and polystyrene/poly(2-chlorostyrene)/deuterated benzene with different polymeric indices  $N$  and polymer concentrations  $c$ . The temperature dependence of the isothermal susceptibility  $S_T$  and the correlation length  $\xi$ , near the stability limit showed the static crossover from the mean-field to the three-dimensional Ising behavior in all solutions. The Ginzburg number  $Gi^{BK}$  was evaluated with the aid of the crossover function of Belyakov and Kiselev. As  $c$  increases from the semidilute region to the bulk limit, the scaled Ginzburg number  $gi^{BK} = Gi^{BK}N$  decreased, with the power  $\alpha$  of  $gi^{BK} \propto c^\alpha$  being  $-1.25$  to  $-2$  as expected by the theory based on the blob concept. The values of  $gi^{BK}(\text{bare})$  evaluated by the bare interactions were smaller than experimental values.

## Introduction

Approaching the critical points, simple or binary fluids exhibit a crossover from the classical mean-field to the three-dimensional Ising (3D Ising) behavior, with changing critical exponents of the thermodynamic properties. This static crossover indicates that the fluctuation of the order parameter becomes infinitely large to be a dominant factor in the thermodynamic behavior. Its location is characterized by the Ginzburg number  $Gi$ , which is a system-dependent parameter. Recently, Belyakov and Kiselev<sup>1,2</sup> have derived a simple universal function describing the static crossover of the isothermal susceptibility in terms of  $Gi$  on the basis of a renormalization-group method with the  $\epsilon$ -expansion.

It was first pointed out by de Gennes<sup>3</sup> that polymeric systems, in particular polymer blends, have a narrower 3D-Ising region and tend to exhibit the mean-field critical behavior. Since then, particular attention has been paid to the crossover behavior in polymeric systems and to the dependence of the Ginzburg number on the polymeric index  $N$  and/or polymer concentration  $c$ . Most of the theoretical<sup>3–7</sup> and experimental<sup>8–18</sup> studies have been devoted to polymer blends. The applicability of Belyakov and Kiselev's universal function has been confirmed for various polymer blends by Meier et al.<sup>15,16</sup> As for semidilute polymer blend solutions, which exhibit a critical behavior mainly due to incompatibility between polymers, Broseta et al.<sup>19</sup> have theoretically studied the crossover behavior on the basis of the blob concept and derived an equation for  $Gi$  as a scaling function of  $c$ .

In polymer blend solutions, which are ternary systems, a small fluctuation of total polymer concentration  $c$  has some influence on the critical behavior, so that a Fisher renormalized Ising region,<sup>21</sup> besides the mean-field and the 3D-Ising regions, must exist in the nearest temperature region to the stability limit. In our previous paper,<sup>20</sup> however, we have experimentally demonstrated that semidilute blend solutions of polymer A/polymer B/good solvent have no Fisher renormalized region in the experimental temperature range, showing a much wider 3D-Ising region than ordinary polymer blend systems. This result is consistent with the



**Figure 1.** Molecular weight–concentration diagram for polystyrene in toluene or benzene, which was deduced from osmotic pressure measurements by Noda et al.<sup>22,23</sup> Symbols represent the blend solutions used in this study: (□) MA1; (■) MA2; (●) CL1; (○) CL2.

theoretical consideration of Broseta et al.,<sup>19</sup> which predicts that the renormalized Ising region is too narrow to be observed under practical experimental conditions. Consequently, we can reasonably suppose a crossover from the 3D-Ising behavior to mean-field behavior for real systems of symmetrical polymer blend solutions.

The Ginzburg number  $Gi$  of a polymer blend solution must monotonously decrease with increasing polymer concentration from the semidilute region, to the concentrated region, to the bulk limit. Needless to say, the polymeric index  $N$  controls  $Gi$  and the boundary of the concentration regions as well. The locations of the concentration regions for polymer solutions are illustrated as a  $c$ –molecular weight ( $M$ ) diagram in Figure 1, which was experimentally determined from osmotic pressure for polystyrene in toluene or benzene by Noda et al.<sup>22,23</sup> The dilute and semidilute regions are separated by the overlap concentration  $c^*$ , which is defined as

$$c^* \equiv \frac{M}{(4/3)\pi\varrho R_F^3 L} \quad (1)$$

Here,  $\varrho$  is polymer density,  $R_F$  is the radius of gyration of a polymer chain in a dilute solution of good solvent, and  $L$  is the Avogadro number. The boundary  $c^{**}$

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between the semidilute and concentrated regions is independent of  $M$  (or  $N$ ). In the semidilute region, the Ginzburg number  $Gi$  is expected to decrease with increasing  $c$ , following a scaling law of  $(c/c^*)^{-1.25}$ .<sup>19</sup> In the concentrated region, it should decrease with a different  $c$  dependence, because the excluded-volume effect is partially screened in the semidilute region, whereas it is entirely screened out in the concentrated region as in the bulk.

In this paper we are concerned with the crossover of the critical behavior in polymer blend solutions over a wide range of total polymer concentration  $c$  and polymeric index  $N$ . The crossover for the isothermal susceptibility  $S_T$  and the correlation length  $\xi_t$  has been investigated by means of static light scattering for four symmetrical polymer blend solutions of different molecular weights and concentrations. We have applied the Belyakov–Kiselev crossover functions<sup>1,2</sup> and evaluated the Ginzburg number  $Gi^{BK}$  to see the  $c$  and  $N$  dependence of  $Gi^{BK}$  over the wide concentration range from the semidilute to the concentrated region and examine the validity of the theoretical prediction based on the blob concept. In the following section, reviewing the theoretical background of the Ginzburg number, we will derive the scaled expressions of  $Gi$  as a function of  $c$  evaluated from the bare interactions, in other words, on the basis of the mean-field descriptions, covering the semidilute, concentrated, and bulk regions. Then we will describe the details of the experiments, give the results, and present a discussion according to the theoretical consideration.

## Theoretical Background

**A. The Ginzburg Number  $Gi$ .** In fluid systems, the critical exponents  $\gamma$  and  $\nu$  for the isothermal susceptibility  $S_T$  and the correlation length  $\xi_T$  are defined through  $S_T \sim \tau^{-\gamma}$  and  $\xi_t \sim \tau^{-\nu}$ , with the reduced temperature  $\tau \equiv |T/T_s - 1|$ , where  $T_s$  is the temperature at the stability limit. On the crossover from the classical mean-field behavior to the 3D-Ising behavior, the values of  $\gamma$  and  $\nu$  vary from  $\gamma = 1$  and  $\nu = 1/2$  to  $\gamma = 1.24$  and  $\nu = 0.63$ ,<sup>24</sup> respectively. The location of the static crossover is specified by the Ginzburg number  $Gi$ : The mean-field theory holds for  $\tau \gg Gi$ , while the 3D-Ising model applies for  $\tau \ll Gi$ .  $Gi$  is given as

$$Gi \sim \frac{b_0^2}{a_0^4} \left( \frac{v_0}{\xi_{t0}^3} \right)^2 \quad (2)$$

with the numerical prefactor depending on the definition. Here  $v_0$  is the volume per molecule, and  $\xi_{t0}$  is the correlation-length amplitude which is of the order of the molecular radius.  $a_0$  and  $b_0$  are the parameters in the Ginzburg–Landau–Wilson expression, eq 3, of free energy  $\Delta f$  near the stability limit.

$$\Delta f(\psi) = \frac{k_B T}{v_0} \int d^3 r \left[ \frac{1}{2} a_0 \tau \psi^2(r) + \frac{1}{4!} b_0 \psi^4(r) + \frac{1}{2} c_0 (\nabla \psi(r))^2 \right] \quad (3)$$

Here,  $k_B$  is the Boltzmann constant and  $\psi(r)$  is the order parameter. The bare interaction parameters  $a_0$  and  $b_0$  are explicitly given in terms of the local free energy density  $f_0$  per volume  $v_0$  of the mean-field expression as

$$a_0 = (\partial^2 \bar{f}_0 / \partial \tau \partial \psi^2) \quad (4)$$

$$b_0 = (\partial^4 \bar{f}_0 / \partial \psi^4) \quad (5)$$

Here,  $\bar{f}_0 = f_0(k_B T/v_0)$  is the reduced free energy, and  $\tau$  is defined as  $\tau \equiv |T/T_{sm} - 1|$  with the mean-field spinodal temperature  $T_{sm}$ . The bare (unrenormalized) amplitude  $\xi_{t0}$  of the correlation length for thermal concentration fluctuations is given by

$$\xi_t = \xi_{t0} \tau^{-1/2} \quad (6)$$

The Ginzburg number  $Gi$ (bare) evaluated from these equations (eqs 4–6) must be proportional to the real  $Gi$  that is evaluated with the renormalized parameters.

**B. Universal Crossover Function.** By the renormalization-group calculation, Belyakov and Kiselev have derived the universal function that describes the static crossover of  $S_T$  for fluids.<sup>1,2</sup> The crossover function is expressed in terms of the Ginzburg number  $Gi^{BK}$  and  $a_0$  as follows.

$$\frac{\tau}{Gi^{BK}} = \{1 + \kappa(S_T a_0 Gi^{BK})^{\Delta/\gamma}\}^{(\gamma-1)/\Delta} \times [(S_T a_0 Gi^{BK})^{-1} + \{1 + \kappa(S_T a_0 Gi^{BK})^{\Delta/\gamma}\}^{-\gamma/\Delta}] \quad (7)$$

$$Gi^{BK} \equiv \frac{b_0^2}{32\pi^4 a_0^4} \left( \frac{v_0}{\xi_{t0}^3} \right)^2 = \left| 1 - \frac{T_{sm}}{T_s} \right| \quad (8)$$

The gap exponent  $\Delta = 0.51$  and the critical exponent  $\gamma = 1.24$  are the values for the 3D-Ising model. The value of the universal constant  $\kappa$  is determined to be 2.333 by  $\epsilon^2$  expansion. The crossover function, eq 7, is a phenomenologically generalized one to reproduce the 3D-Ising behavior at the limit of  $\tau/Gi^{BK} \ll 1$  as follows.

$$S_T^{-1} = \frac{\kappa^{\gamma/\Delta} a_0 (Gi^{BK})^{1-\gamma}}{(1 + \kappa^{\gamma/\Delta})^\gamma} \tau^\gamma \quad (3D\text{-Ising}; \tau/Gi^{BK} \ll 1) \quad (9)$$

Equations 7 and 9 and a presumable mean-field behavior are illustrated in Figure 2, along with the locations of  $T_s$  and  $T_{sm}$ .

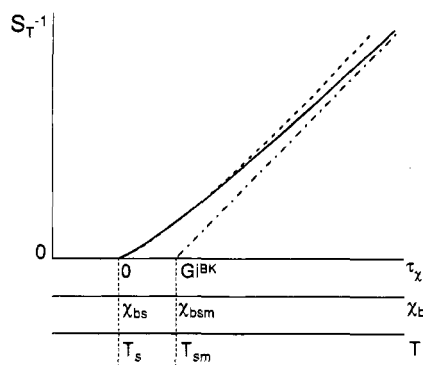
**C.  $Gi^{BK}$ (bare) for Polymer Blend Solutions with a Blob Model.** Here, we will evaluate  $Gi^{BK}$ (bare) for a polymer A/polymer B/good solvent system with a blob picture to estimate the  $N$  and  $c$  dependence of the Ginzburg number  $Gi$ . By the use of the blob concept, the system is approximated by binary mixtures of Gaussian chains of blobs. In describing the quasi-binary mixture with the blob model, we impose the basic assumption that the blob volume  $v_b(c)$  is common for the two polymers. Furthermore, the segment volume  $v_s$ , independent of  $c$ , is commonly defined for unlike polymers. Then, since  $v_b(c)$  is written by

$$v_b(c) = v_s g(c)/c \quad (10)$$

the number  $g(c)$  of segments within a blob is also common for polymers A and B. Using the segment volume  $v_s$ , the polymeric indices  $N_A$  and  $N_B$  are defined by

$$N_A = v_A/v_s, \quad N_B = v_B/v_s \quad (11)$$

where  $v_i$  is the volume of an  $i$ -polymer molecule. Then, the mean-field expression of the local free energy density



**Figure 2.** Schematic illustration of the static crossover for the isothermal susceptibility  $S_T$ : solid line, the Belyakov–Kiselev crossover function (eq 7); dashed line, the asymptotic Ising behavior (eq 9); broken line, the presumable mean-field behavior.

$f_{b0}$  per  $v_b(c)$  is given by<sup>19</sup>

$$\bar{f}_{b0} = \frac{f_{b0}}{k_B T / v_b} = \frac{\phi_A}{N_A/g} \ln \phi_A + \frac{\phi_B}{N_B/g} \ln \phi_B + \chi_b \phi_A \phi_B \quad (12)$$

where  $\phi_i$  is the volume fraction of polymer  $i$  in the total volume of polymers ( $\phi_A + \phi_B = 1$ ), which corresponds to the order parameter  $\psi(r)$ .  $\chi_b$  represents the Flory–Huggins interaction parameter between unlike blobs.  $\chi_b$  depends on temperature and the concentration  $c$  and is here assumed independent of the composition  $\phi_i$ .

The reduced interaction parameter  $\tau_\chi$  is defined by

$$\tau_\chi \equiv \left| 1 - \frac{\chi_b}{\chi_{bs}} \right| \quad (13)$$

and the mean-field definition

$$\tau_{\chi m} \equiv \left| 1 - \frac{\chi_b}{\chi_{bsm}} \right| \quad (14)$$

Here,  $\chi_{bs}$  and  $\chi_{bsm}$  are  $\chi_b$  at the actual spinodal temperature  $T_s$  and the mean-field spinodal temperature  $T_{sm}$ , respectively. It is noteworthy that  $\chi_b$  has a different dependence on the polymer concentration  $c$  between the semidilute and concentrated regions. However, as far as we are observing the phenomena as a function of  $\tau_\chi$ , the  $c$  dependence of  $\chi_b$  does not appear in the formalism of the critical behavior explicitly.

From eqs 4 and 5 with eq 12, the bare constants  $a_0$  and  $b_0$  are derived as

$$a_0 = \frac{1}{(N_A/g)\phi_A} + \frac{1}{(N_B/g)\phi_B} = 2\chi_{bsm} = \left( \frac{\phi_A \phi_B \langle N \rangle}{g} \right)^{-1} \quad (15)$$

$$b_0 = 2 \left( \frac{1}{(N_A/g)\phi_A^3} + \frac{1}{(N_B/g)\phi_B^3} \right) = 2 \left( \frac{\phi_A \phi_B \langle N \rangle}{\langle \phi^{-2} \rangle g} \right)^{-1} \quad (16)$$

The random phase approximation for binary polymer mixtures yields the bare amplitude  $\xi_{t0}$  for the present model as<sup>10</sup>

$$\xi_{t0} = \frac{1}{(3a_0)^{1/2}} \left( \frac{R_{gA}^2(c)}{(N_A/g)\phi_A} + \frac{R_{gB}^2(c)}{(N_B/g)\phi_B} \right)^{1/2} = \left( \frac{R_g^2(c)}{3} \right)^{1/2} \quad (17)$$

$\langle N \rangle$ ,  $\langle \phi^{-2} \rangle$ , and  $\langle R_g^2(c) \rangle$  in eqs 15–17 are defined as follows.

$$\langle N \rangle = \frac{\phi_A^{-1} + \phi_B^{-1}}{N_A^{-1}\phi_A^{-1} + N_B^{-1}\phi_B^{-1}} \quad (18)$$

$$\langle \phi^{-2} \rangle = \frac{N_A^{-1}\phi_A^{-3} + N_B^{-1}\phi_B^{-3}}{N_A^{-1}\phi_A^{-1} + N_B^{-1}\phi_B^{-1}} \quad (19)$$

$$\langle R_g^2(c) \rangle = \frac{R_{gA}^2(c)N_A^{-1}\phi_A^{-1} + R_{gB}^2(c)N_B^{-1}\phi_B^{-1}}{N_A^{-1}\phi_A^{-1} + N_B^{-1}\phi_B^{-1}} \quad (20)$$

Here, the subscripts A and B denote polymers A and B, respectively.  $\langle N \rangle$  is alternatively written as

$$\langle N \rangle = \langle v \rangle / v_s \quad (21)$$

where the mean volume  $\langle v \rangle$  of the polymer molecules is given by

$$\langle v \rangle = \left[ \frac{v_A^{-1}\phi_A^{-1} + v_B^{-1}\phi_B^{-1}}{\phi_A^{-1} + \phi_B^{-1}} \right]^{-1} \quad (22)$$

Then, the bare Ginzburg number  $Gi^{BK}(\text{bare})$  is evaluated by eq 8 with eqs 10 and 15–17 to be

$$Gi^{BK}(\text{bare}) = \frac{27}{8\pi^2} f_\phi v_s^2 \langle R_g^2(c) \rangle^{-3} \langle N \rangle^2 c^{-2} \quad (23)$$

where the asymmetry factor  $f_\phi$  for the composition is defined as

$$f_\phi = \phi_A^2 \phi_B^2 \langle \phi^{-2} \rangle^2 \quad (24)$$

which becomes unity when  $\phi_A = \phi_B = 1/2$ .

Now, the segment volume  $v_s$  is defined as

$$v_s = \langle v \rangle^3 / \langle R_{g\theta}^2 \rangle^3 \quad (25)$$

with

$$\langle R_{g\theta}^2 \rangle = \frac{R_{g\theta A}^2 v_A^{-1} \phi_A^{-1} + R_{g\theta B}^2 v_B^{-1} \phi_B^{-1}}{v_A^{-1} \phi_A^{-1} + v_B^{-1} \phi_B^{-1}} \quad (26)$$

where  $R_{g\theta i}$  is the unperturbed radius of gyration of an  $i$ -polymer molecule. Once the segment size  $v_s$  is definitely defined by eq 25,  $N_A$ ,  $N_B$ ,  $\langle N \rangle$ , and  $g$  are uniquely defined and cannot arbitrarily be taken hereafter.

By the scaling law,  $\langle R_g^2(c) \rangle$  for the semidilute region ( $c^* < c < c^{**}$ ) is described as

$$\langle R_g^2(c) \rangle = \langle R_{g\theta}^2 \rangle \left( \frac{c}{c^{**}} \right)^{-(2\sigma-1)/(3\sigma-1)} \quad (c^* < c < c^{**}) \quad (27)$$

where  $\sigma \approx 0.588$  is the swelling exponent defined by  $R_F \sim N^\sigma$ . A detailed discussion on the expression of  $\langle R_g^2(c) \rangle$  and  $c^{**}$  may be found in the Appendix. For the concentrated region ( $c^{**} < c < 1$ ) including the bulk limit,

$$\langle R_g^2(c) \rangle = \langle R_{g\theta}^2 \rangle \quad (c^{**} < c < 1) \quad (28)$$

Using eqs 25–28, one can rewrite eq 23 to obtain the expressions of  $Gi^{BK}(\text{bare})$  for the semidilute solution, the concentrated solution, and the bulk limit.

$$Gi^{\text{BK}}(\text{bare}) = \frac{27}{8\pi^4} f_\phi (c^{**})^{-3(2\sigma-1)/(3\sigma-1)} \langle N \rangle^{-1} c^{-1/(3\sigma-1)} \quad (c^* < c < c^{**}) \quad (29)$$

$$= \frac{27}{8\pi^4} f_\phi \langle N \rangle^{-1} c^{-2} \quad (c^{**} < c < 1) \quad (30)$$

$$= \frac{27}{8\pi^4} f_\phi \langle N \rangle^{-1} \quad (\text{bulk}) \quad (31)$$

Under the symmetrical conditions, i.e.,  $N_A = N_B = N$  and  $\phi = 1/2$ , eq 29 is reduced to be the following equation written in terms of  $c/c^*$  with the coefficient  $K_R$  used by Broseta et al.<sup>19</sup> (see Appendix)

$$Gi^{\text{BK}}(\text{bare}) = \frac{6}{\pi^2 K_R} \left( \frac{c}{c^*} \right)^{-1/(3\sigma-1)} \quad (c^* < c < c^{**}) \quad (32)$$

Equation 32 is equivalent to the equation of Broseta et al. (see a note in ref 19). Bates et al.<sup>11,12</sup> defined the Ginzburg number  $Gi^\circ$  as

$$Gi^\circ \equiv \left| 1 - \frac{\chi_x}{\chi_{\text{sm}}} \right| \quad (33)$$

$\chi_x$  is the interaction parameter  $\chi$  at which the asymptotic  $S_T^{-1} - \chi$  curve for the mean-field behavior intersects with that for the Ising behavior, and  $\chi_{\text{sm}}$  is  $\chi$  at the mean-field spinodal temperature. They have derived a theoretical expression equivalent to eq 31, which is related to the present  $Gi^{\text{BK}}(\text{bare})$  by

$$Gi^\circ = \tilde{C} f_\phi \langle N \rangle^{-1} = \frac{8\pi^4}{27} \tilde{C} Gi^{\text{BK}}(\text{bare}) \quad (\text{bulk}) \quad (34)$$

where  $\tilde{C}$  is the constant.

The Ginzburg number may have a  $f_\phi \langle N \rangle^{-1}$  dependence in all regions, so that if a scaled Ginzburg number  $gi$  is defined as

$$gi^{\text{BK}} \equiv \frac{Gi^{\text{BK}} \langle N \rangle}{f_\phi} \quad (35)$$

then  $gi^{\text{BK}}(\text{bare})$  can be expressed by

$$gi^{\text{BK}}(\text{bare}) = \frac{27}{8\pi^4} (c^{**})^{-3(2\sigma-1)/(3\sigma-1)} c^{-1/(3\sigma-1)} \quad (c^* < c < c^{**}) \quad (36)$$

$$= \frac{27}{8\pi^4} c^{-2} \quad (c^{**} < c < 1) \quad (37)$$

$$= \frac{27}{8\pi^4} \quad (\text{bulk}) \quad (38)$$

It should be pointed out that since  $c^{**}$  is independent of  $N$ ,  $gi^{\text{BK}}$  is a function of  $c$  alone, irrespective of  $N$ , over the semidilute and concentrated regions. Therefore, plots of  $gi^{\text{BK}}$  vs  $c$  for different  $N$  and  $c$  make a master curve, following eqs 36–38, as long as  $c^{**}$  can be regarded as a constant for the set of data.

## Experimental Section

**Materials.** Weight-average molecular weight  $M_w$  and polydispersity index  $M_w/M_n$  are listed in Table 1 for polystyrene (PS), poly(methyl methacrylate) (PMMA), and poly(2-chlorostyrene) (P2ClS), along with material

codes and sources. Numbers in the material codes refer to the molecular weight in ten kilograms per mole.

**Samples.** Blend solutions used were PS/PMMA/deuterated benzene (Bnz- $d_6$ ) solutions and PS/P2ClS/Bnz- $d_6$  solutions, all of which had a lower critical solution temperature. Two polymer components in respective blend solutions had approximately the same molecular weight, and benzene- $d_6$  was thermodynamically good for PS, PMMA, and P2ClS. Polymer compositions ( $\phi_{\text{PS}}$ ) of the samples prepared were close to the critical composition predicted by the Flory–Huggins theory (eq 12). They might not be real critical compositions, but solutions of these compositions could reach a temperature sufficiently close to the stability limit with no phase separation. Details of sample preparation were described in the previous paper.<sup>20</sup> Sample codes and characteristics of the blend solutions are listed in Table 2.  $M_w$  and total polymer concentration  $c$  of blend solutions are also shown in Figure 1. Samples MA1 and MA2 belong to the semidilute region, while CL1 and CL2 fall within the concentrated region.

**Light Scattering.** Details of the light scattering apparatus were described elsewhere.<sup>25</sup> An Ar ion laser operated at the wavelength 488 nm was used as a light source. A sample tube of 4.2 mm inner diameter was immersed in a thermostated ( $\pm 0.05$  °C) index-matching oil bath. The scattered light intensity  $I(q)$  was measured by the photon-counting method as a function of length  $q$  of the scattering vector. Turbidity attenuation and the multiple scattering effect were estimated from the Rayleigh ratio of scattered light intensity to be less than  $2 \times 10^{-2}$  of the observed intensity,<sup>20</sup> so no corrections for them were made.

In a polymer/polymer/solvent system, the scattered light intensity  $I(q)$  can be expressed as a sum of structure functions  $S_{ij}(q) = \langle \delta c_i(q) \delta c_j(-q) \rangle$  weighted with the refractive index increment, where  $\delta c_i(q)$  is the Fourier transform of concentration fluctuations of component  $i$ . However, all structure functions show a similar critical divergence near the stability limit irrespective of  $ij$ . For a symmetrical system such as the present case, where both polymers have similar polymeric indices and the solvent is sufficiently good for both, quasi-binary treatment is feasible and the critical divergence is governed by fluctuations of the polymer composition. Actually, the scattered light intensity from binary solutions PS/Bnz- $d_6$  with concentration 0.07–0.22 vol/vol was 1/50 to 1/1000 times of that of used blend solutions, so most of scattered light intensity may come from polymer-composition fluctuations. Thus, the inverse isothermal susceptibility  $S_T^{-1}$  and the correlation length  $\xi_t$  of polymer-composition fluctuations were evaluated from  $I(q)$  by the least-squares fitting to the Ornstein–Zernike equation, eq 39:

$$\frac{I(q)}{I(0)} = (1 + q^2 \xi_t^2)^{-1} \quad (39)$$

$I(0)$  provides  $S_T^{-1}$  in an arbitrary scale by  $S_T^{-1} \sim T/I(0)$ .<sup>20</sup> As examples of the good linearity between  $I^{-1}(q)$  and  $q^2$ , the results for sample MA1 are shown in Figure 3a. However, the most concentrated solution CL1 exhibited excess intensity deviating from the linearity in the smaller  $q$  range as shown in Figure 3b, probably because there remained some heterogeneity in composition owing to their high viscosity. Thus, we had evaluated  $S_T^{-1}$  and  $\xi_t$  for CL1 by the fitting of  $I(q)$  at higher  $q$  ( $q^2 > 3.8 \times 10^{-4} \text{ nm}^{-2}$ ).

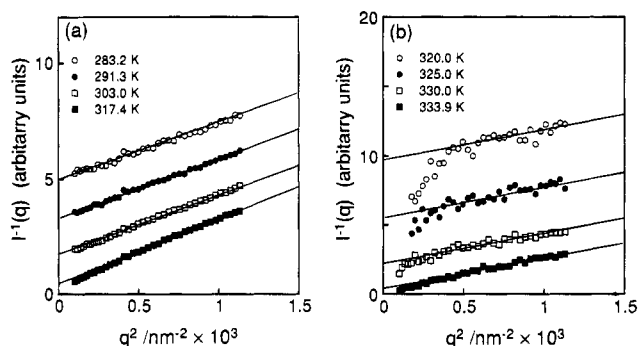
**Table 1. Weight-Average Molecular Weight and Polydispersity Index of the Polymers Used in This Study**

material code	$M_w \times 10^{-5}$	$M_w/M_n$	note
polystyrene			
PS10	10.0	$\leq 1.06$	a product of Pressure Chemicals
PS36	35.5	1.02	a product of Tosoh
PS126	126	1.05	a product of Tosoh
poly(methyl methacrylate)			
PMMA33	32.7	$\leq 1.10$	a product of Pressure Chemicals
PMMA109	109	1.08	radical polymerized
poly(2-chlorostyrene)			
P2ClS12	12.4	1.19	radical polymerized
P2ClS37	36.9	1.23	radical polymerized

**Table 2. Characteristics of Polymer Blend Solutions**

sample code	system	$\phi_{PS}$	$c/vol\%$ ( $c/c^*$ ) <sup>a</sup>	$\langle N \rangle$	$\langle R_g^2(c) \rangle^{1/2}/nm^b$	$f_\phi$
MA1	PS36/PMMA33/Bnz- <i>d</i> <sub>6</sub>	0.484	7.82 (8.52)	75.8	21.0	1.01
MA2	PS127/PMMA109/Bnz- <i>d</i> <sub>6</sub>	0.497	4.33 (12.7)	259	41.8	1.00
CL1	PS10/P2ClS12/Bnz- <i>d</i> <sub>6</sub>	0.469	48.9 (19.7)	17.5	9.1	1.06
CL2	PS36/P2ClS37/Bnz- <i>d</i> <sub>6</sub>	0.452	21.8 (23.8)	58.7	18.2	1.08

<sup>a</sup> The values of  $c/c^*$  were calculated with the swelling radius  $R_F$  (eq 40) and the molecular weight  $M_w$  for PS. <sup>b</sup> Calculated by eqs 26–28 with  $c^{**} = 0.538$  vol/vol-solution,  $\sigma = 0.595$ , and the published data<sup>26</sup> for the unperturbed radius  $R_{g0}$ .

**Figure 3.** Ornstein-Zernike plots of  $I^{-1}(q)$  vs  $q^2$  for blend solutions: (a) MA1; (b) CL1.

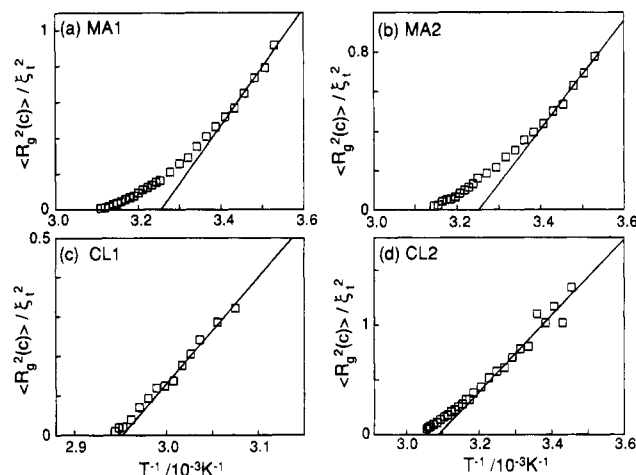
## Results and Discussion

For data presentation and analysis, we first evaluated  $v_A$ ,  $v_B$ , and  $v_s$  for each blend solution to calculate the values of  $\langle N \rangle$ ,  $\langle R_g^2(c) \rangle$ , and  $f_\phi$ . The volume  $v_i$  was calculated from  $v_i = M_{wi}/\rho_L$  with the density  $\rho = 1.065$  g/cm<sup>3</sup> for PS, and then the value of  $v_s$  was obtained from eqs 22, 25, and 26 with reported data<sup>26</sup> for the unperturbed radius  $R_{g0}/M_w^{1/2}$ . The values of  $\langle N \rangle$  and  $f_\phi$  for blend solutions were calculated by eqs 18, 19, and 24 and are summarized in Table 2. To evaluate  $\langle R_g^2(c) \rangle$  as a function of concentration from eqs 27 and 28, the value of  $c^{**}$  was estimated from eq A17 as follows.  $K_1$  was first estimated on the basis of eq A4 (see Appendix) by using the following expressions for  $R_F$  and  $R_{g0}$  of the PS chain obtained by Miyaki et al.<sup>27</sup>

$$\overline{R_F^2}/cm^2 = (1.47 \pm 0.05) \times 10^{-18} M_w^{1.19 \pm 0.05} \quad (40)$$

$$\overline{R_{g0}^2}/cm^2 = (8.8 \pm 0.2) \times 10^{-18} M_w \quad (41)$$

The value of  $K_1$  obtained was 1.27, which was approximately the same as those evaluated for PMMA and P2ClS. Then  $c^{**}$  was determined from eq A17 with  $g_0 = 1$  and  $K_1 = 1.27$  to be 0.538 vol/vol-solution. Eventually, the values of  $\langle R_g^2(c) \rangle$  were calculated from eqs 26–28 with the  $c^{**}$  value and  $\sigma = 0.595$  which was taken so as to be consistent with eq 40. The value of  $c^{**} = 0.538$  vol/vol-solution is much larger than  $c^{**} = 0.14$ – $0.19$  vol/vol-solution determined from osmotic pressure by Noda et al.<sup>22,23</sup> However, the value of  $c^{**}$  obtained here is consistent with those estimated from direct

**Figure 4.** Temperature dependence near the stability limit of the reduced correlation length  $\langle R_g^2(c) \rangle/\xi_t^2$  for samples: (a) MA1; (b) MA2; (c) CL1; (d) CL2. Full lines represent the results of fittings of eq 42 to the mean-field regions.

measurements of chain dimensions for PS in toluene solutions<sup>28</sup> and for polyisoprene in good solvent solutions.<sup>29,30</sup>

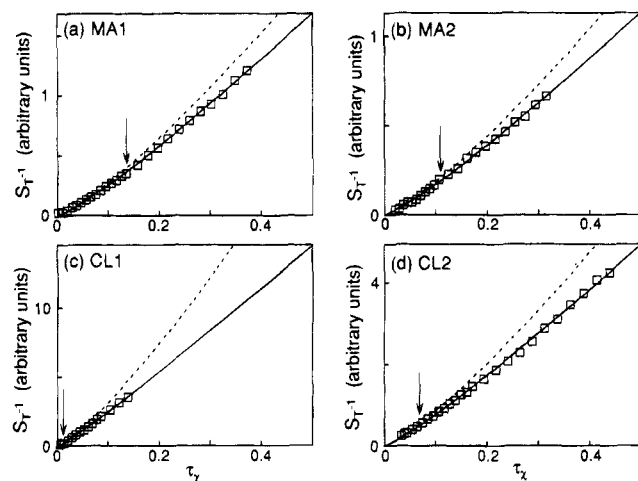
Figure 4 presents the temperature dependence of the correlation length  $\xi_t$  near the stability limit as plots of  $\langle R_g^2(c) \rangle/\xi_t^2$  vs  $T^{-1}$ . In all solutions,  $\xi_t$  shows the crossover from the linear region at lower temperatures to the concave region at higher temperatures, which is consistent with the static crossover from the classical mean-field behavior  $\xi_t \sim \tau_\chi^{-1/2}$  to the 3D-Ising behavior  $\xi_t \sim \tau_\chi^{-0.63}$ . Describing the temperature dependence of  $\chi_b$  as  $\chi_b = A - bT^{-1}$  ( $A, b > 0$ ), the following expression for the mean-field region was derived from eqs 6, 14, and 17.

$$\frac{\langle R_g^2(c) \rangle}{\xi_t^2} = 3 \left| 1 - \frac{\chi_b}{\chi_{bsm}} \right| = \left( \frac{3b}{\chi_{bsm}} \right) \left| \frac{1}{T} - \frac{1}{T_{sm}} \right| \quad (42)$$

Although the experimental range may not fully cover the mean-field region, we assumed that the linear region at lower temperatures in Figure 4 was described by eq 42 and estimated the values of  $\chi_{bsm}/b$  and  $T_{sm}$  by the least-squares fittings to the linear region. From both values the temperature dependence of  $\chi_b$  was evaluated to be of the form  $\chi_b/b = A/b - T^{-1}$ . The obtained values of  $A/b$ ,  $\chi_{bsm}/b$ , and  $T_{sm}$  are listed in Table 3.

Table 3. Static Critical Properties of Polymer Blend Solutions

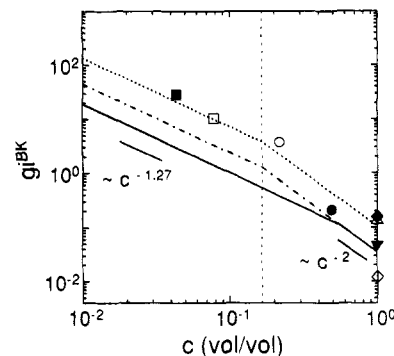
sample code	$(A/b) \times 10^3$	$(\chi_{bsm}/b) \times 10^3$	$T_{sm}/K$	$(\chi_{bs}/b) \times 10^3$	$T_g/K$	$G_i^{BK}$	$g_i^{BK}$
MA1	4.17 <sub>8</sub>	0.92 <sub>3</sub>	307.2	1.07 <sub>0</sub>	321.7	0.137	10.1
MA2	4.34 <sub>1</sub>	1.08 <sub>9</sub>	307.5	1.22 <sub>1</sub>	320.6	0.109	28.1
CL1	4.11 <sub>4</sub>	1.11 <sub>1</sub>	333.1	1.12 <sub>6</sub>	334.7	0.0128	0.221
CL2	3.94 <sub>8</sub>	0.85 <sub>9</sub>	323.7	0.92 <sub>4</sub>	330.5	0.0688	3.73



**Figure 5.** Dependence of the inverse isothermal susceptibility  $S_T^{-1}$  on the reduced interaction parameter  $\tau_\chi$  for samples: (a) MA1; (b) MA2; (c) CL1; (d) CL2. Solid lines, the fitting results of the universal crossover function (eq 7); dashed line, the asymptotic Ising behavior (eq 9); arrows, the Ginzburg number  $G_i^{BK}$ .

Replacing  $\tau$ ,  $T_{sm}$ , and  $T_s$  in eqs 7–9 by  $\tau_\chi$ ,  $\chi_{bsm}$ , and  $\chi_{bs}$ , respectively, the universal crossover function (eq 7 with eqs 8 and 9) was fitted to the experimental  $I(0)/T$  vs  $T$  relation to obtain the Ginzburg number  $G_i^{BK}$ . Here the fitting parameters were  $T_s$  and a scale factor for  $S_T$  because the experimental  $S_T$  was given in an arbitrary scale.  $T_s$  provided  $G_i^{BK}$  and  $\tau_\chi$ . Figure 5 shows the temperature dependence of the isothermal susceptibility  $S_T$  for all blend solutions as plots of  $S_T^{-1}$  vs  $\tau_\chi$ . Full lines, dashed lines, and arrows in the plots represent the universal crossover function, the asymptotic Ising behavior, and the redefined Ginzburg number  $G_i^{BK}$ , respectively. Although the present fitting ranges of  $\tau_\chi$  ( $< 0.4$ ) and  $G_i^{BK}$  ( $= 0.07$ – $0.14$ ) do not sufficiently satisfy the required conditions ( $\tau_\chi \ll 1$  and  $G_i^{BK} \ll 1$ ) for the crossover function,<sup>31</sup> it describes the experimental data of all solutions well. It should be noted here that, in the fitting to the crossover function,  $T_{sm}$  was fixed at the value determined on the basis of eq 42 in Figure 4. Therefore, the  $G_i^{BK}$  values obtained are not fully based on the fitting to the Belyakov–Kiselev crossover function, but rely on the  $T_{sm}$  evaluation as well and involve uncertainties in these two determining processes. Probably, the value of  $G_i^{BK}$  evaluated here may primarily depend on the  $T_{sm}$  evaluation and may have slightly been underestimated. The obtained values of  $\chi_{bs}/b$ ,  $T_s$ , and  $G_i^{BK}$  are also listed in Table 3.

The scaled Ginzburg number  $g_i^{BK}$  was plotted against the concentration  $c$  in log–log scales over the semidilute and concentrated regions in Figure 6. Also plotted were the results reported for symmetrical and asymmetrical bulk polymer blends.<sup>10–12,14,15</sup> The values of  $\langle N \rangle$  and  $f_\phi$  for the respective samples were estimated in the same way as for the present systems. The solid line in the figure represents the bare Ginzburg number  $g_i^{BK}(\text{bare})$  of eqs 36–38 with  $\sigma = 0.595$  and  $c^{**} = 0.538$  vol/vol-solution, and the broken line represents the  $g_i^{BK}(\text{bare})$  calculated with  $c^{**} = 0.165$  vol/vol-solution, which is the



**Figure 6.** Double-logarithmic plots of the scaled Ginzburg number  $g_i^{BK}$  vs  $c$ . Symbols: ( $\square$ ), ( $\blacksquare$ ), ( $\bullet$ ), and ( $\circ$ ) are the same as in Figure 1; ( $\blacklozenge$ ), ( $\triangle$ ) polyisoprene/poly(ethylene–propylene) blends (Stepanek et al.<sup>11,12</sup>); ( $\blacktriangledown$ ) poly(dimethylsiloxane)/poly(ethylmethylsiloxane) blends (Meier et al.<sup>14</sup>); ( $\diamond$ ), deuterated polystyrene/poly(vinyl methyl ether) blends (Schwahn et al.<sup>10,15,16</sup>). Solid and broken lines represent the bare Ginzburg number  $g_i^{BK}(\text{bare})$  of eqs 36–38 with  $c^{**} = 0.538$  and  $0.165$  vol/vol-solution, respectively. Dotted line represents the calculated curve that was obtained by vertically shifting the broken line [ $g_i^{BK}(\text{bare})$  with  $c^{**} = 0.165$  vol/vol-solution] such that it agreed with the experimental data for blend solutions best.

mean value of  $c^{**}$  estimated by Noda et al.<sup>22,23</sup> The experimental value of  $g_i^{BK}$  for the systems with different  $\langle N \rangle$  decreases with increasing polymer concentration monotonously as expected from the theoretical consideration in the Introduction. The strength of the concentration dependence is close to that predicted from  $g_i^{BK}(\text{bare})$  with  $c^{**} = 0.165$  vol/vol-solution, being approximately described by the vertically shifted line (dotted line) of  $g_i^{BK}(\text{bare})$  with  $c^{**} = 0.165$  vol/vol-solution.

Poor agreement in the concentration dependence was found between  $g_i^{BK}$  and  $g_i^{BK}(\text{bare})$  with  $c^{**} = 0.538$  vol/vol which was estimated from  $R_g(c)$  behavior. The Ginzburg number appears to show the crossover from the semidilute to the concentrated behavior around the same concentration  $c^{**}$  as osmotic pressure<sup>22,23</sup> and viscosity<sup>32,33</sup> do. We may have to keep in mind that the screening of excluded-volume effects in the blend solution is not always the same as in the pure solution, since, in the present treatment  $\langle R_g^2(c) \rangle$  has been evaluated on the basis of knowledge of pure polymer solution.

$g_i^{BK}$  are much larger than  $g_i^{BK}(\text{bare})$ . This may be attributed primarily to a breakdown of the mean-field treatment near the critical point and possibly to the incompressibility approximation.<sup>5,6</sup> For various bulk blends, Meier et al.<sup>14</sup> reported that the experimental values of  $a_0$  and  $b_0$  were larger than the mean-field values and the deviation for  $b_0$  was larger than that for  $a_0$ , which is consistent with the present results.

The vertically shifted line of  $g_i^{BK}$  with  $c^{**} = 0.165$  vol/vol is extrapolated to the bulk limit to a value around 0.1, which falls in the range of reported values for bulk blends. The universality of  $g_i^{BK}$  for bulk polymer blends is expected from the fixed value of  $g_i^{BK}(\text{bare}) = 27/8\pi^4 = 0.035$ . However,  $g_i^{BK}$  at the bulk blend limit show some scatter as illustrated in Figure 6, suggesting a system dependence of  $g_i^{BK}$ . The reported values of  $g_i^{BK}$

(in bulk) range from 0.019 to 0.158. The universal constant  $\tilde{C}$  in the expression of Bates et al.<sup>11,12</sup> (eq 34) was also reported to have system-dependent values, that is,  $\tilde{C} = 0.016\text{--}2.03$ .<sup>10,17</sup> More experimental studies on the Ginzburg number  $Gi$  for blends and blend solutions by the use of the universal crossover function are needed to examine the universality of  $gi^{\text{BK}}$ .

## Appendix

**A. Expressions for  $\langle R_g^2(c) \rangle$  and  $c^{**}$ .** The screening of excluded-volume effects on the chain dimensions over the semidilute, concentrated, and bulk regions has not thoroughly been revealed for a blend solution consisting of unlike polymers with different Kuhn lengths. Therefore, in the present treatment, the blob size is assumed common for unlike polymers, and the segment size is commonly defined such that

$$\langle R_{g\theta}^2 \rangle = v_s^{2/3} \langle N \rangle \quad (\text{A1})$$

which defines the polymeric indices  $N_i$  and  $g$  uniquely. The blob radius  $R_b$  must be proportional to  $v_s^{1/3} g^\sigma$ , so we put  $R_b^2 = v_s^{2/3} g^{2\sigma} / K_1$  with a common constant  $K_1$  for  $i = A$  and  $B$ , since the blob volume  $v_b$  is the same for unlike polymers. Then for the semidilute region, one has

$$R_{gi}^2(c) = \frac{v_s^{2/3} g^{2\sigma} (N_i)}{K_1} \quad (\text{A2})$$

which leads to

$$\langle R_g^2(c) \rangle = \frac{v_s^{2/3} g^{2\sigma} \langle N \rangle}{K_1} \quad (\text{A3})$$

(see eq 20), or using eq A1,

$$\langle R_g^2(c) \rangle = \langle R_{g\theta}^2 \rangle g^{2\sigma-1} K_1^{-1} \quad (\text{A4})$$

$K_1$  is a system-dependent constant, reflecting the stiffness of the polymer molecules. According to the scaling law, the polymeric index  $g(c)$  of a blob has the following  $c$  dependence.<sup>34,35</sup>

$$g = K_g c^{-1/(3\sigma-1)} \quad (\text{A5})$$

$K_g$  is also a system-dependent constant. Equations A4 and A5 provide the following expression of  $\langle R_g^2(c) \rangle$  as a function of  $c$ :

$$\langle R_g^2(c) \rangle = \langle R_{g\theta}^2 \rangle K_1^{-1} K_g^{2\sigma-1} c^{-(2\sigma-1)/(3\sigma-1)} \quad (\text{A6})$$

In the concentrated region, since the excluded-volume effect is assumed to be completely screened out, the chain dimension is the unperturbed one, independent of  $c$ :

$$\langle R_g^2(c) \rangle = \langle R_{g\theta}^2 \rangle \quad (\text{A7})$$

Then, assuming a continuous change of  $\langle R_g^2(c) \rangle$  at the crossover concentration  $c^{**}$ , one can obtain the following relationship among  $K_1$ ,  $K_g$ , and  $c^{**}$  from eqs A6 and A7.

$$(c^{**})^{-(2\sigma-1)/(3\sigma-1)} = K_1 K_g^{1-2\sigma} \quad (\text{A8})$$

This relation with eq A6 leads to the following scaling equations, which is a direct consequence of the scaling

law with the continuous change of  $\langle R_g^2(c) \rangle$  at  $c^{**}$ .

$$\frac{\langle R_g^2(c) \rangle}{\langle R_{g\theta}^2 \rangle} = \left( \frac{c}{c^{**}} \right)^{-(2\sigma-1)/(3\sigma-1)} \quad (c^{**} < c < c^{**}) \quad (\text{A9})$$

$$= 1 \quad (c^{**} < c < 1) \quad (\text{A10})$$

In the treatment of Broseta et al.,<sup>19,36</sup> the scaling formula for  $\langle R_g^2(c) \rangle$  was given for the symmetrical system by

$$\frac{R_g^2(c)}{R_F^2} = K_R \left( \frac{c}{c^*} \right)^{-(2\sigma-1)/(3\sigma-1)} \quad (\text{A11})$$

Noting that  $R_F^2 = v_s^{2/3} N^{2\sigma} / K_1$ ,  $c^*$  is expressed from the definition of  $c^*$  (eq 1) as

$$c^* = \frac{3}{4\pi} K_1^{3/2} N^{1-3\sigma} \quad (\text{A12})$$

and consequently, one has

$$\frac{R_g^2(c)}{R_F^2} = K_R \left( \frac{4}{3} \pi K_1^{-3/2} \right)^{(2\sigma-1)/(3\sigma-1)} N^{1-2\sigma} c^{-(2\sigma-1)/(3\sigma-1)} \quad (\text{A13})$$

Then, noticing that if  $N = g$ , then  $R_g^2(c)/R_F^2 = 1$ , and comparing eq A13 with eq A5, one has the relation

$$K_g = K_R^{1/(2\sigma-1)} \left( \frac{3}{4\pi} K_1^{3/2} \right)^{1/(3\sigma-1)} \quad (\text{A14})$$

Using eqs A8, A12, and A14, eq 29 in the text can be rewritten in terms of  $c/c^*$  as eq 32 for the symmetrical system.

**B. Evaluations of  $K_1$ ,  $K_g$ , and  $c^{**}$ .** On the basis of eq A4 with  $g = N$ , the constant  $K_1$  can be estimated from the values of the swelling radius  $R_F$  in a good solvent and the unperturbed radius  $R_{g\theta}$  in a  $\Theta$  solvent and/or in bulk obtained experimentally. Then,  $c^{**}$  can be estimated as a concentration of the crossover for  $R_g(c)$  in the following two ways.

(i) The value of  $K_R$  was theoretically given by Broseta et al.<sup>36,37</sup> to be about 1.4. Equations A8 and A14 with this value yield

$$c^{**} = \frac{3}{4\pi} K_R^{(3\sigma-1)/(2\sigma-1)} K_1^{-1/2(2\sigma-1)} = 0.92 K_1^{-1/2(2\sigma-1)} \quad (\text{A15})$$

(ii) In the concentrated region, the scaling law gives<sup>34,35</sup>

$$g = g_0 c^{-2} \quad (\text{A16})$$

From the continuity of  $R_g^2(c)$  at  $c^{**}$ , eq A4 with  $g = g_0(c^{**})^{-2}$  leads to the following relation.

$$c^{**} = g_0^{1/2} K_1^{-1/2(2\sigma-1)} \quad (\text{A17})$$

If it is assumed that  $g = 1$  in bulk, i.e., at  $c = 1$ , then one can put  $g_0 = 1$ . Under this assumption, the prefactor  $g_0^{1/2}$  of eq A17 becomes unity, which is very close to the prefactor of eq A15, 0.92.

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- where  $\eta$  is the composition difference between the coexisting phases at the same  $\tau_\chi$  in the two-phase region. From the definition and relations  $S_T^{-1} = a_0\tau_\chi/v_b$ ,  $\xi_t = \xi_{t0}\tau_\chi^{-1/2}$ , and  $\eta = 2(6a_0/b_0)^{1/2}\tau_\chi^{1/2}$ ,  $\tau_\chi^*$  is given in terms of the present parameters as  $\tau_\chi^* = (b_0^2/36a_0^4)(v_b/\xi_{t0}^3)^2$ , which leads to the relation  $Gi^{BK} = (9/8\pi^4)\tau_\chi^*$ . This reproduces eq 32.
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$$\tau_\chi^* = \frac{16\pi^2}{3K_R^3} \left( \frac{c}{c^*} \right)^{-1/(3\sigma-1)}$$

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